

STABLE IMPLEMENTATION OF BOUNDARY CONDITIONS FOR DGSEM APPROXIMATION OF THE COMPRESSIBLE EULER AND NAVIER-STOKES EQUATIONS

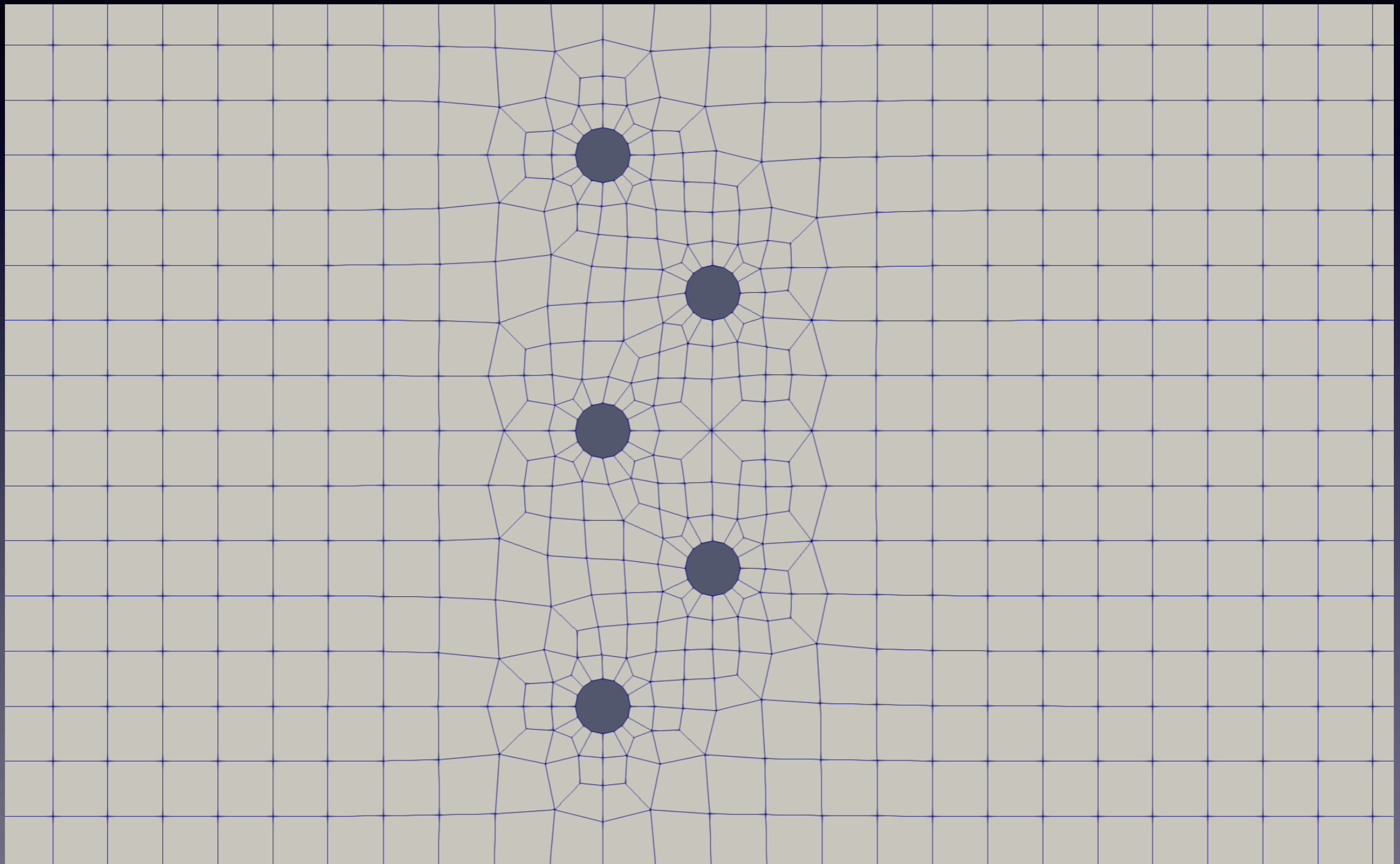
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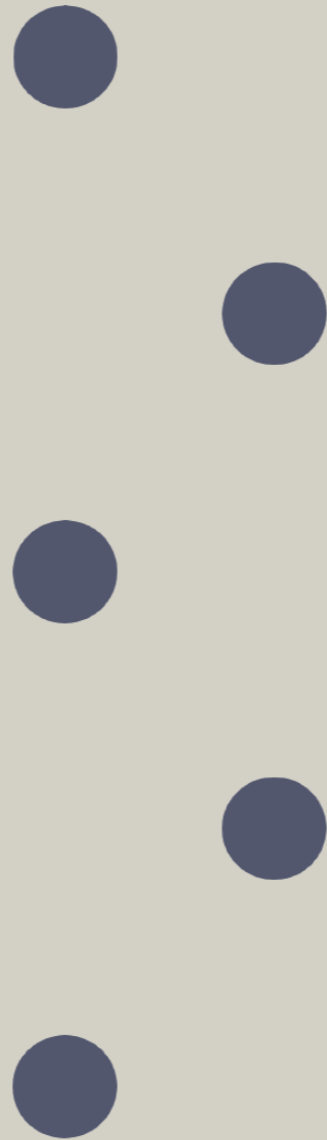
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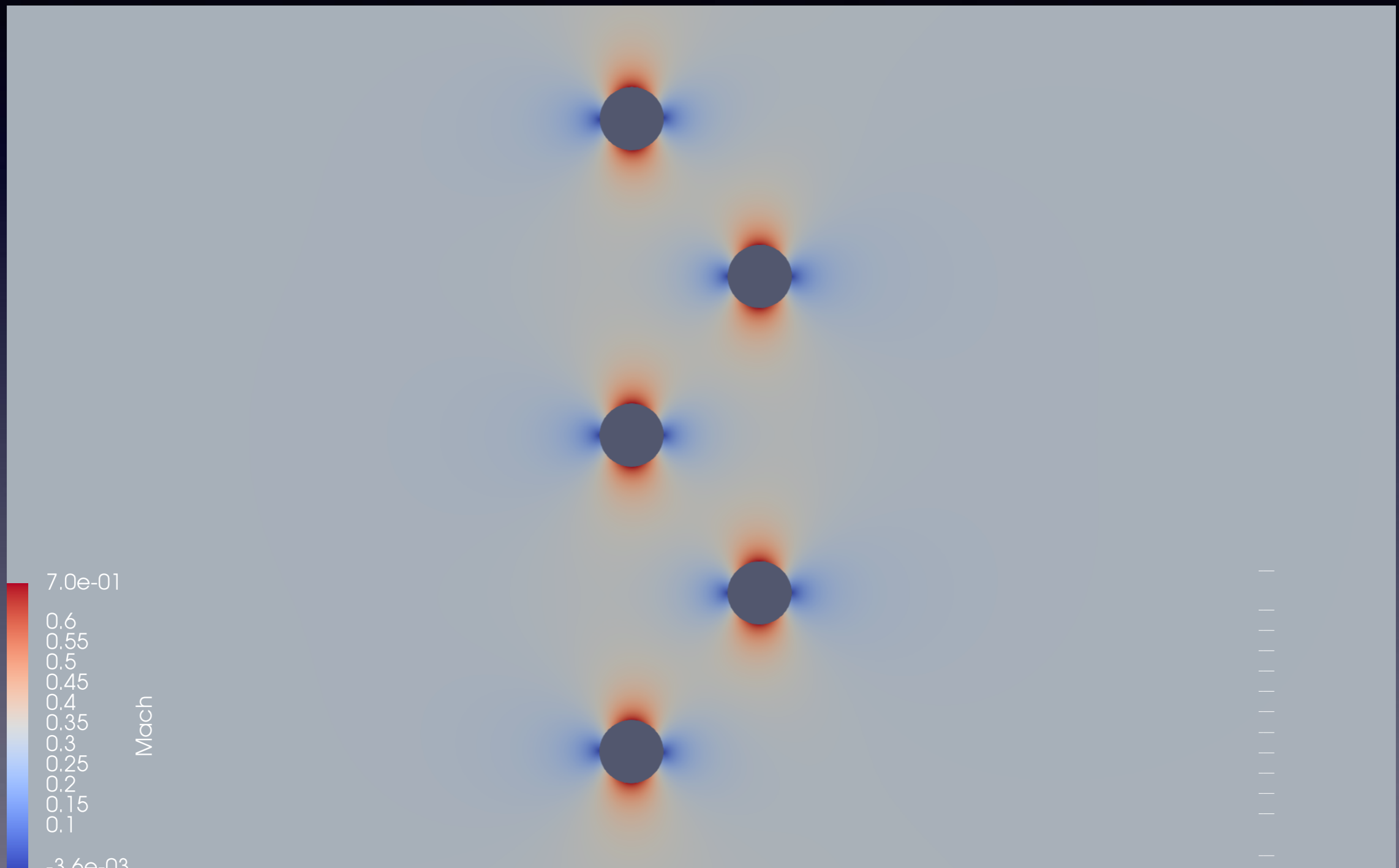
A Flow Geometry



A Compressible Flow



Another Compressible Flow



Boundary Conditions Determine the Flow!

Yet:

- Hardly discussed except in passing
- Often dealt with in ad-hoc manner
- Published proposals not stable

We study...

- Conditions under which DGSEMs are stable
- Examples of stable BC implementations
- General Analysis
 - 3D
 - Curved Elements
 - Linear and nonlinear equations

Compressible Flow Model

Navier-Stokes Equations: Conservative form

$$\mathbf{u}_t + \sum_{i=1}^3 \frac{\partial \mathbf{f}_i}{\partial x_i} = \frac{1}{\text{Re}} \sum_{i=1}^3 \frac{\partial \mathbf{f}_{v,i}(\mathbf{u}, \nabla_x \mathbf{u})}{\partial x_i}$$

Conservative Variables

$$\mathbf{u} = \begin{bmatrix} \rho \\ \rho \vec{v} \\ \rho E \end{bmatrix} = \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ \rho w \\ \rho E \end{bmatrix}$$

Compact Version

$$\mathbf{u}_t + \vec{\nabla}_x \cdot \overleftrightarrow{\mathbf{f}} = \frac{1}{\text{Re}} \vec{\nabla}_x \cdot \overleftrightarrow{\mathbf{f}}_v \left(\mathbf{u}, \vec{\nabla}_x \mathbf{u} \right)$$

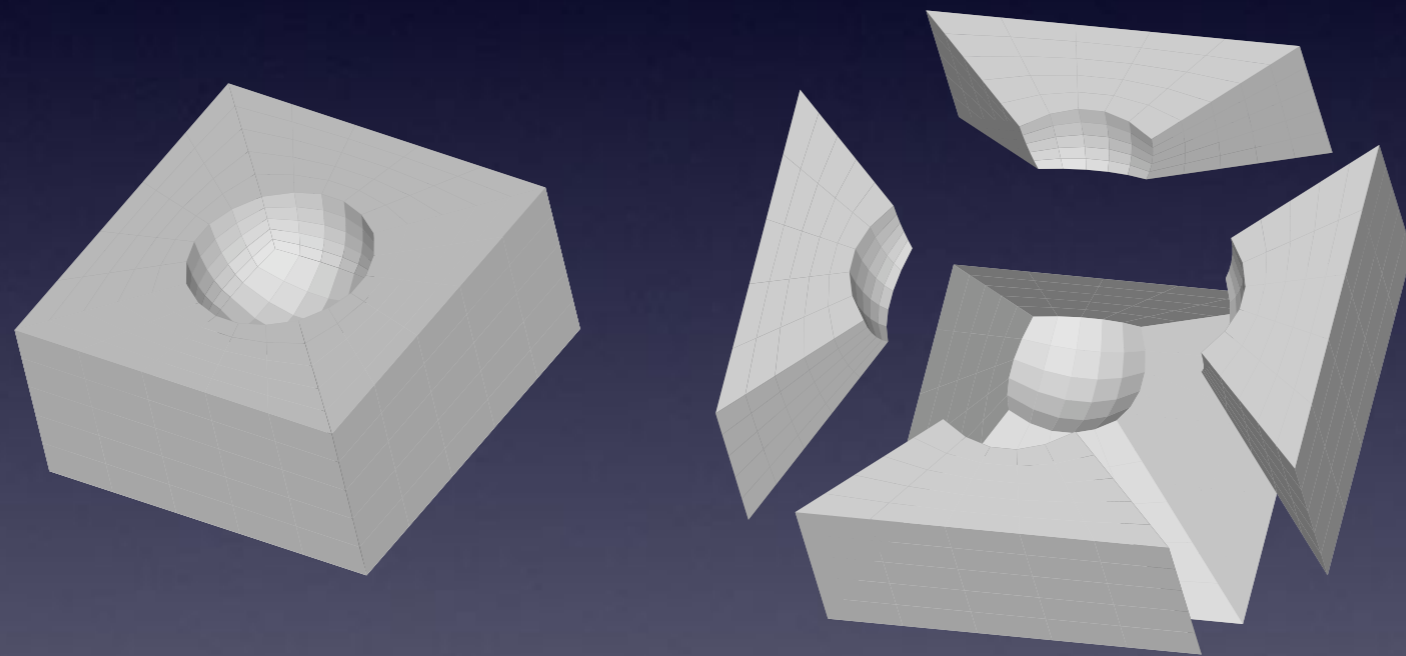
Vector of Vectors: $\overleftrightarrow{\mathbf{f}} = \begin{bmatrix} \mathbf{f}_1 \\ \mathbf{f}_2 \\ \mathbf{f}_3 \end{bmatrix}$

Write as 1st order system with

$$\overleftrightarrow{\mathbf{q}} = \vec{\nabla}_x \mathbf{u}$$

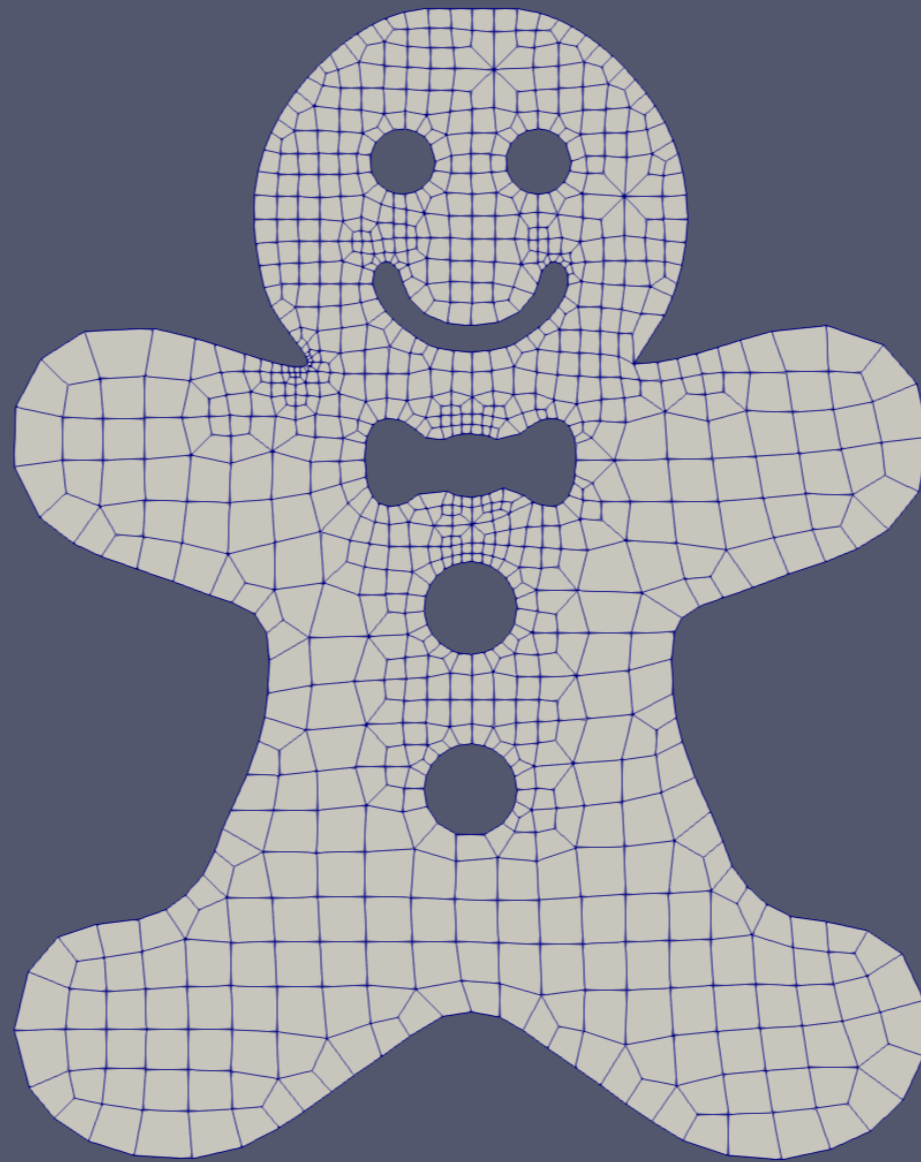
DGSEM Approximation

Subdivide domain into elements

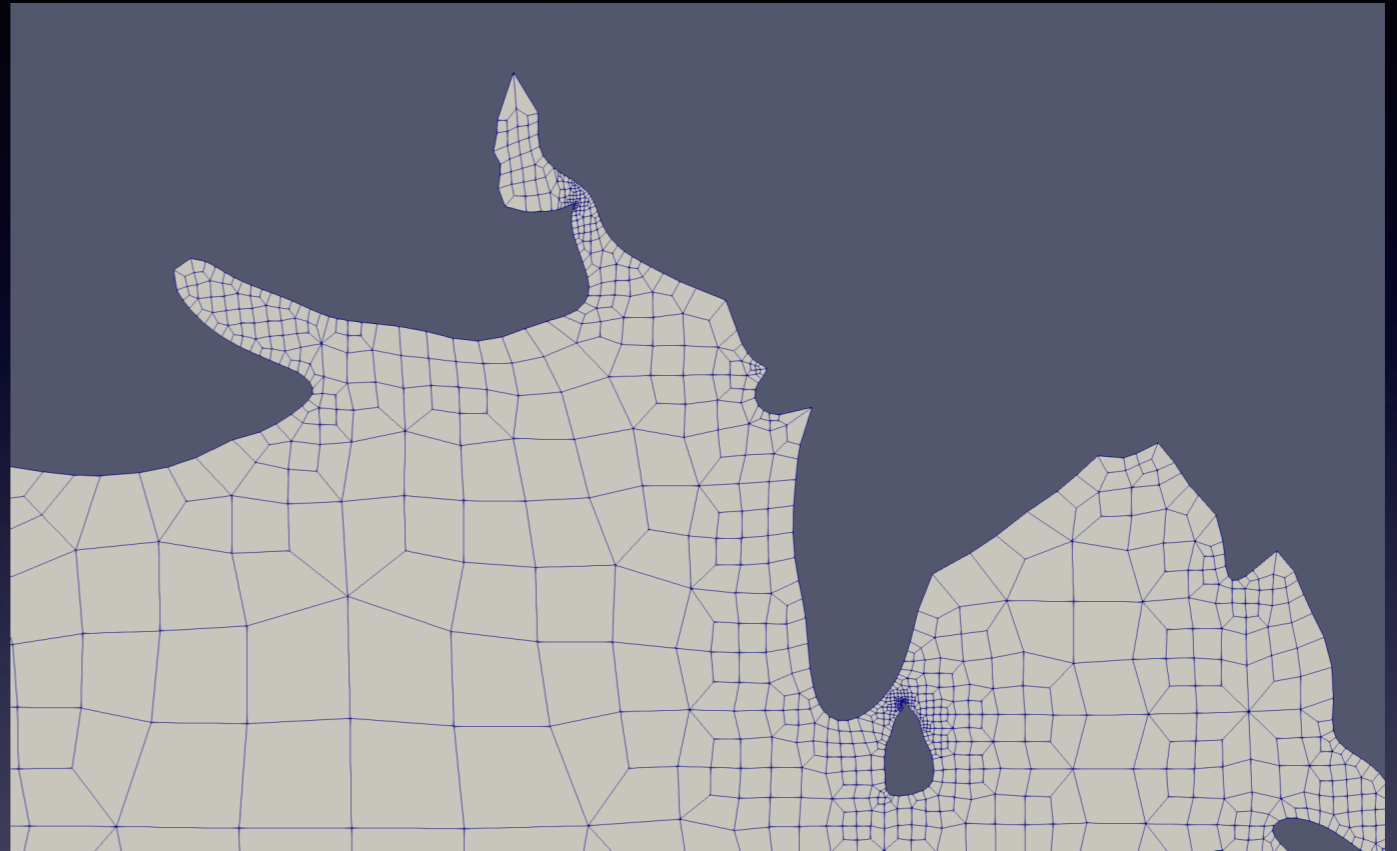
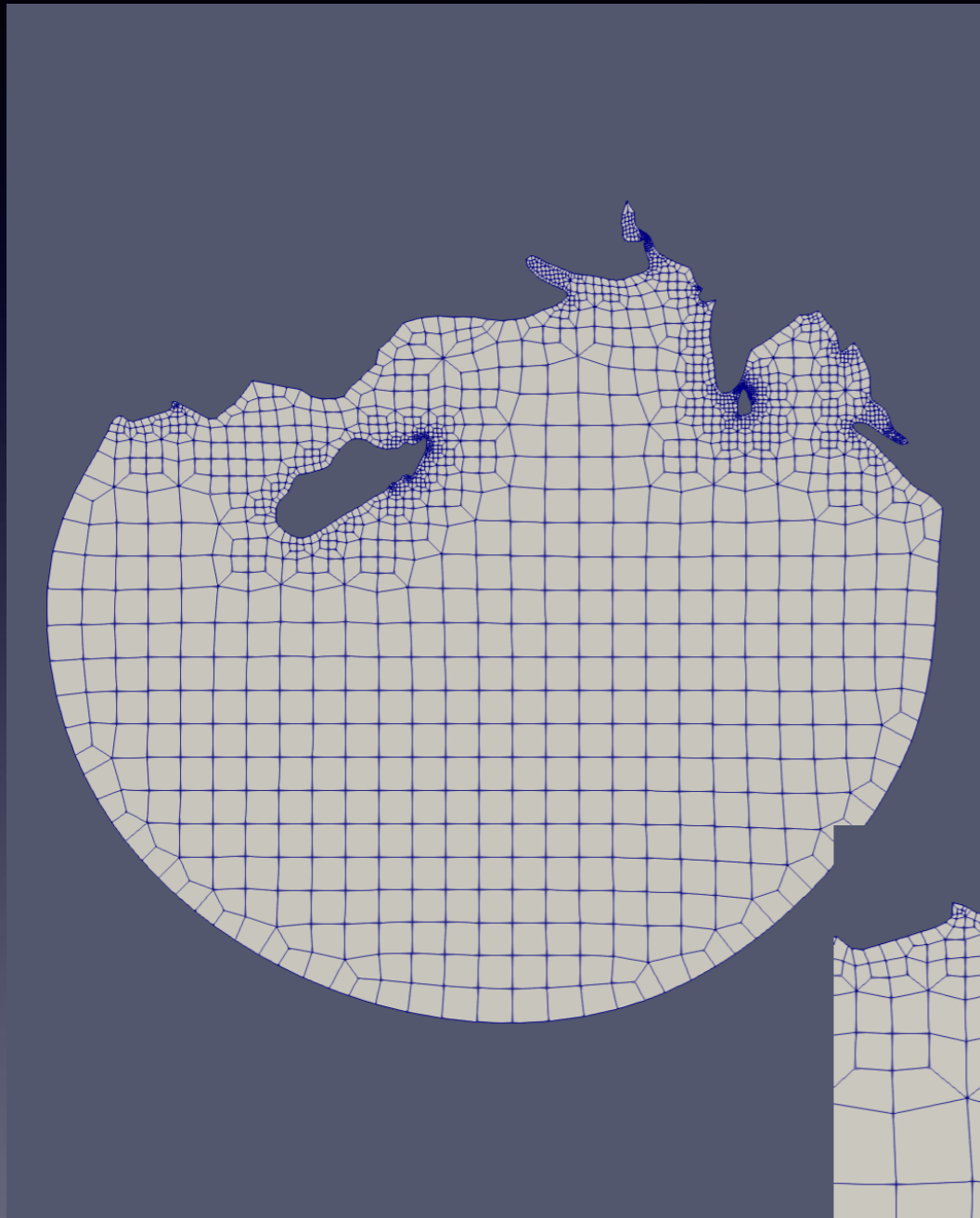


Curved Elements OK!

Unstructured Grids OK

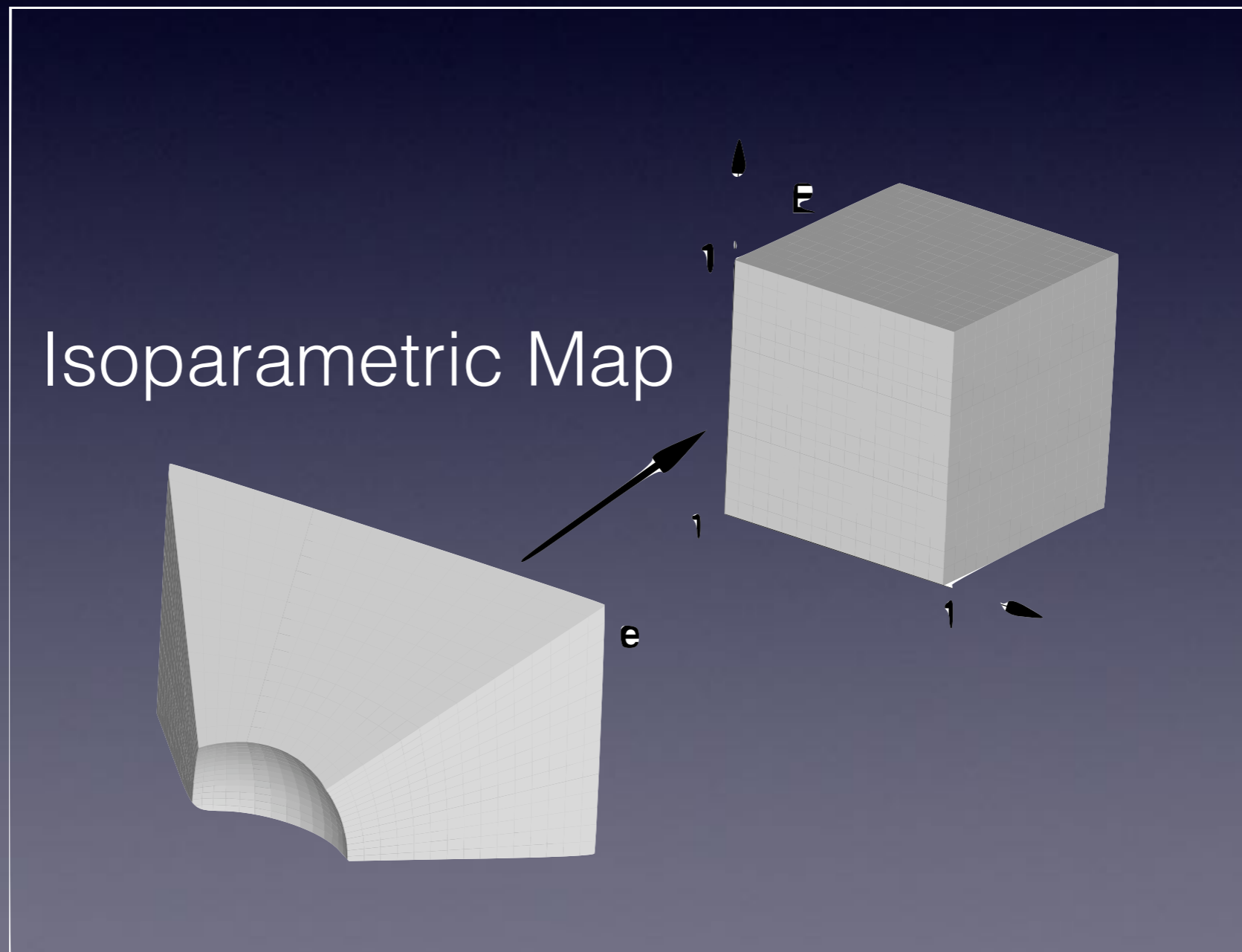


Unstructured Grids OK



DGSEM Approximation

Map Element to Reference Element



Transformation of Operators

$$\vec{a}_i = \frac{\partial \vec{X}}{\partial \xi^i} \quad i = 1, 2, 3$$

$$\mathcal{J} \vec{a}^i = \vec{a}_j \times \vec{a}_k, \quad (i, j, k) \text{ cyclic}$$

Gradient

$$\vec{\nabla}_x \mathbf{u} = \begin{bmatrix} \mathbf{u}_x \\ \mathbf{u}_y \\ \mathbf{u}_z \end{bmatrix} = \frac{1}{\mathcal{J}} \begin{bmatrix} \mathcal{J} a_1^1 \mathbf{I}_5 & \mathcal{J} a_1^2 \mathbf{I}_5 & \mathcal{J} a_1^3 \mathbf{I}_5 \\ \mathcal{J} a_2^1 \mathbf{I}_5 & \mathcal{J} a_2^2 \mathbf{I}_5 & \mathcal{J} a_2^3 \mathbf{I}_5 \\ \mathcal{J} a_3^1 \mathbf{I}_5 & \mathcal{J} a_3^2 \mathbf{I}_5 & \mathcal{J} a_3^3 \mathbf{I}_5 \end{bmatrix} \begin{bmatrix} \mathbf{u}_\xi \\ \mathbf{u}_\eta \\ \mathbf{u}_\zeta \end{bmatrix} = \frac{1}{\mathcal{J}} \mathcal{M} \vec{\nabla}_\xi \mathbf{u}$$

Divergence

$$\vec{\nabla}_x \cdot \overleftrightarrow{\mathbf{g}} = \frac{1}{\mathcal{J}} \vec{\nabla}_\xi \cdot (\mathcal{M}^T \overleftrightarrow{\mathbf{g}})$$

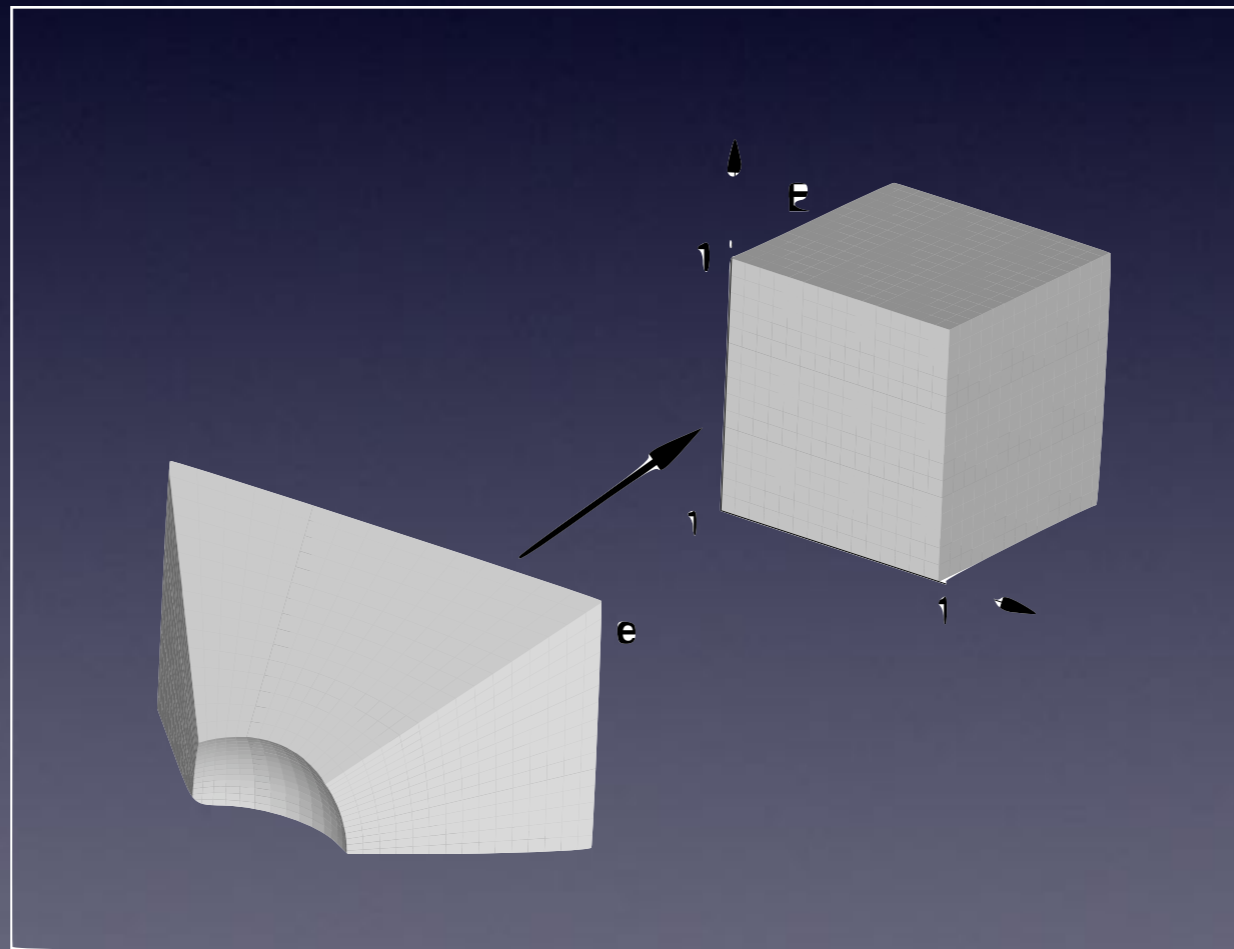
Define Contravariant fluxes:

$$\overleftrightarrow{\tilde{\mathbf{f}}} = \mathcal{M}^T \overleftrightarrow{\mathbf{f}}$$

NS in Reference Coordinates

$$\mathcal{J} \mathbf{u}_t + \vec{\nabla}_\xi \cdot \vec{\mathbf{f}} = \frac{1}{\text{Re}} \vec{\nabla}_\xi \cdot \vec{\mathbf{f}}_v (\mathbf{u}, \vec{\mathbf{q}})$$

$$\mathcal{J} \vec{\mathbf{q}} = \mathcal{M} \vec{\nabla}_\xi \mathbf{u}$$



$$\mathbf{u}_t + \vec{\nabla}_x \cdot \vec{\mathbf{f}} = \frac{1}{\text{Re}} \vec{\nabla}_x \cdot \vec{\mathbf{f}}_v \left(\mathbf{u}, \vec{\nabla}_x \mathbf{u} \right)$$

$$\vec{\mathbf{q}} = \vec{\nabla}_x \mathbf{u}$$

Weak Form Construction

$$\mathcal{J}\mathbf{u}_t + \vec{\nabla}_\xi \cdot \vec{\tilde{\mathbf{f}}} = \frac{1}{\text{Re}} \vec{\nabla}_\xi \cdot \vec{\tilde{\mathbf{f}}}_v (\mathbf{u}, \vec{\mathbf{q}})$$

$$\mathcal{J}\vec{\mathbf{q}} = \mathcal{M}\vec{\nabla}_\xi \mathbf{u}$$

(1) Take inner product of equations with test functions

$$\langle u, v \rangle = \int_E uv dE$$

(2) Apply Gauss Law

$$\langle \mathcal{J}\mathbf{u}, \phi \rangle + \int_{\partial E} \phi^T \left\{ \vec{\tilde{\mathbf{f}}} - \frac{1}{\text{Re}} \vec{\tilde{\mathbf{f}}}_v \right\} \cdot \hat{n} \, dS - \langle \vec{\tilde{\mathbf{f}}}, \vec{\nabla}_\xi \phi \rangle = -\frac{1}{\text{Re}} \langle \vec{\tilde{\mathbf{f}}}_v, \vec{\nabla} \phi \rangle$$

$$\langle \mathcal{J}\vec{\mathbf{q}}, \vec{\psi} \rangle = \int_{\partial E} \mathbf{u}^T \left\{ \mathcal{M}^T \vec{\psi} \right\} \cdot \hat{n} \, dS - \langle \mathbf{u}, \vec{\nabla} \cdot (\mathcal{M}^T \vec{\psi}) \rangle$$

Approximate

Functions with polynomials

Boundary quantities
with numerical ones

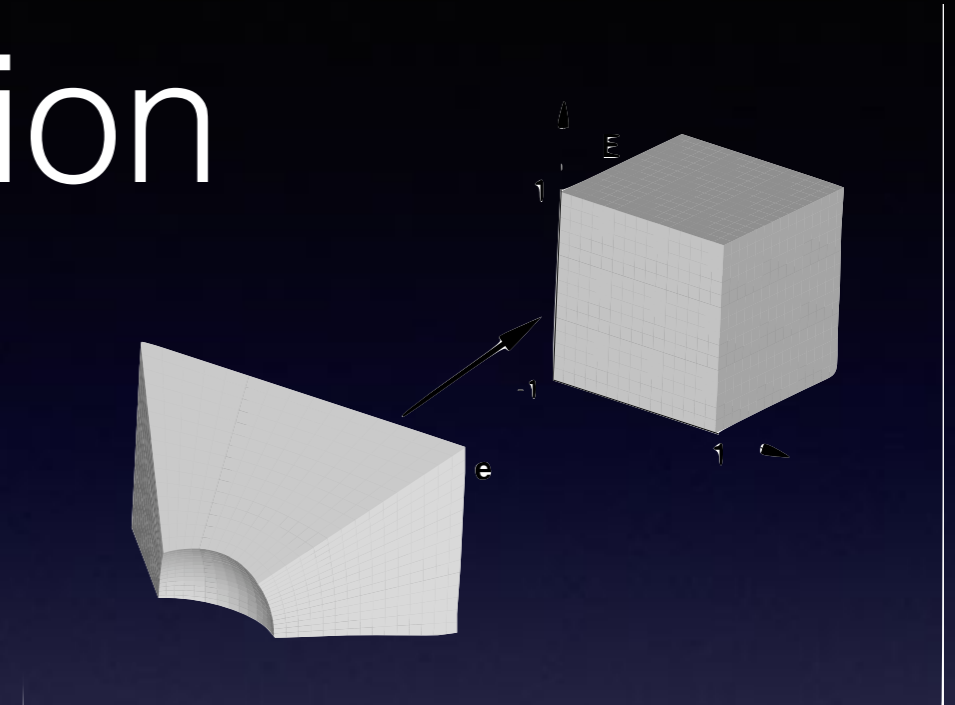
$$\langle \mathcal{J}\mathbf{u}, \phi \rangle + \int_{\partial E} \phi^T \left\{ \tilde{\mathbf{f}} - \frac{1}{\text{Re}} \tilde{\mathbf{f}}_v \right\} \cdot \hat{\mathbf{n}} \, dS - \langle \tilde{\mathbf{f}}, \vec{\nabla}_\xi \phi \rangle = -\frac{1}{\text{Re}} \langle \tilde{\mathbf{f}}_v, \vec{\nabla} \phi \rangle$$

$$\langle \mathcal{J}\tilde{\mathbf{q}}, \tilde{\boldsymbol{\psi}} \rangle = \int_{\partial E} \mathbf{u}^T \left\{ \mathcal{M}^T \tilde{\boldsymbol{\psi}} \right\} \cdot \hat{\mathbf{n}} \, dS - \langle \mathbf{u}, \vec{\nabla} \cdot (\mathcal{M}^T \tilde{\boldsymbol{\psi}}) \rangle$$

Integrals
with quadrature

Continuous Function Approximation

Approximation by Polynomial Interpolant



$$U \left(\vec{\xi} \right) = \mathbb{I}^N (u) = \sum_{i,j,k=0}^N u \left(\xi_i, \eta_j, \zeta_k \right) \ell_i \left(\xi \right) \ell_j \left(\eta \right) \ell_k \left(\zeta \right)$$

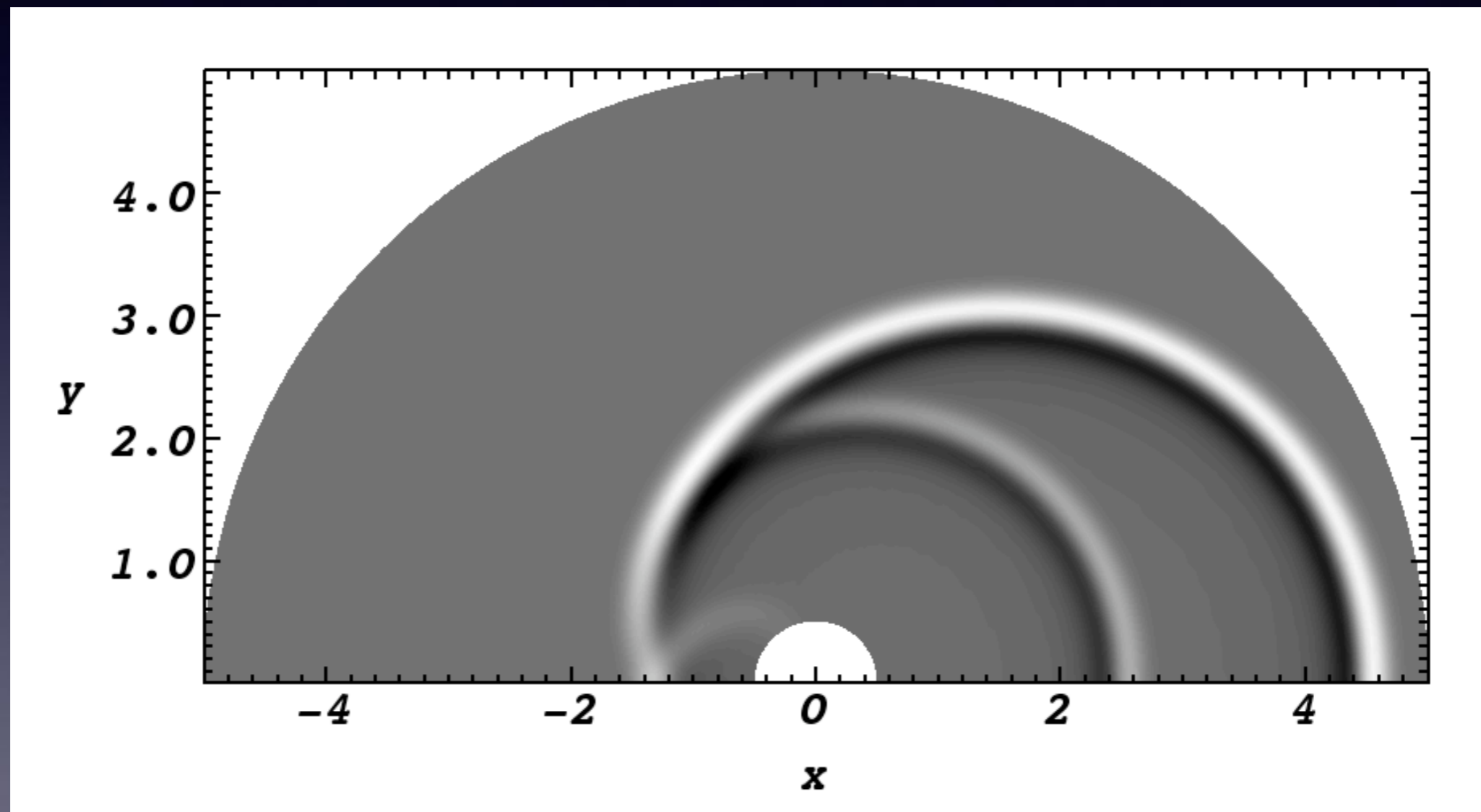
$$\ell_j(x) = \prod_{i=0; i \neq j}^N \frac{x - x_i}{x - x_j} = \text{Lagrange Interpolating Polynomial of degree } N$$

$x_j = \text{Gauss Lobatto points}$

$$\ell_j(x_i) = \delta_{ij}$$

Arbitrary High Order

Acoustic Scattering from a Cylinder



74th Order

Differentiation

Differentiate interpolant, evaluate at quadrature points

$$\begin{aligned}\frac{\partial U}{\partial \xi} \Big|_{nml} &= \sum_{i,j,k=0}^N u_{ijk} \ell'_i(\xi_n) \ell_j(\eta_m) \ell_k(\zeta_l) \\ &= \sum_{i=0}^N u_{ijk} \ell'_i(\xi_n) = \sum_{i=0}^N u_{ijk} \mathcal{D}_{ni}\end{aligned}$$

Differentiation

Gradient

$$\nabla U_{ijk} = \sum_{n=0}^N U_{njk} \mathcal{D}_{in} \hat{\xi} + \sum_{n=0}^N U_{ink} \mathcal{D}_{jn} \hat{\eta} + \sum_{n=0}^N U_{ijn} \mathcal{D}_{kn} \hat{\zeta}$$

Divergence

$$\nabla \cdot \vec{F}_{ijk} = \sum_{n=0}^N F_{njk}^{(\xi)} \mathcal{D}_{in} + \sum_{n=0}^N F_{ink}^{(\eta)} \mathcal{D}_{jn} + \sum_{n=0}^N F_{ijn}^{(\zeta)} \mathcal{D}_{kn}$$

Integral Approximation

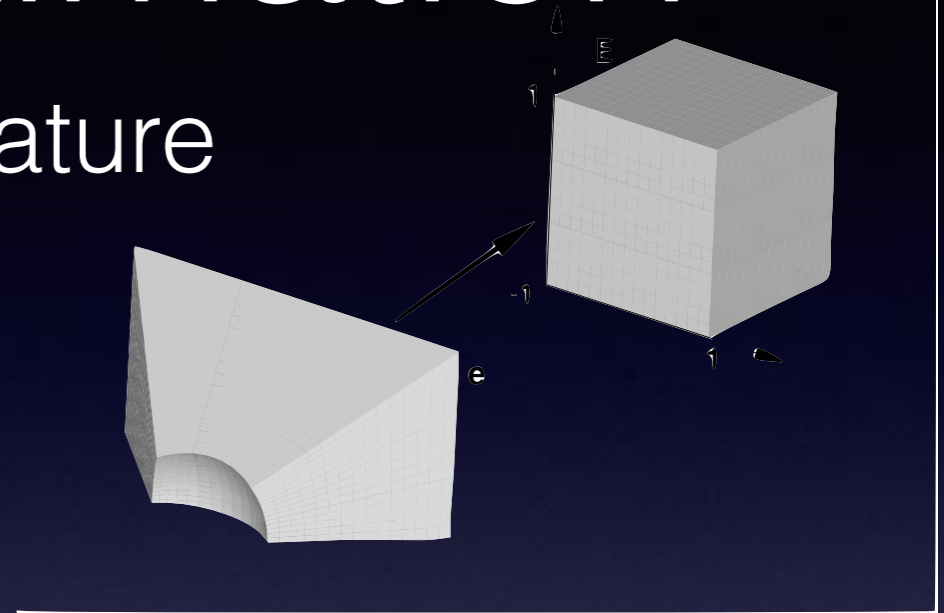
Gauss-Lobatto Quadrature

Integration over Volume

$$\int_{E,N} g d\xi d\eta d\zeta \equiv \sum_{i,j,k=0}^N g_{ijk} w_{ijk}, \quad (w_{ijk} = w_i w_j w_k)$$

Defines discrete inner product/Norm

$$\langle U, V \rangle_N \equiv \int_{E,N} UV d\xi d\eta d\zeta = \sum_{i,j,k=0}^N U_{ijk} V_{ijk} w_{ijk}$$



Summation-By-Parts

Exactness of Gauss Quadrature implies

Integration By Parts

$$(u, v_\xi) = \int_{\partial E} UV \Big|_{\xi=-1}^1 d\eta d\zeta - (u_\xi, v)$$



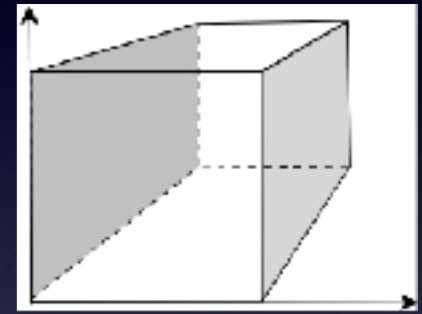
Summation by Parts

$$(U, V_\xi)_N = \int_{\partial E, N} UV \Big|_{\xi=-1}^1 d\eta d\zeta - (U_\xi, V)_N$$

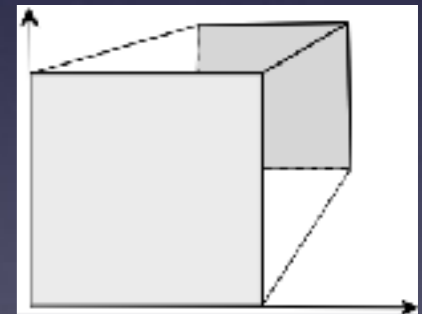
Summation by Parts

works in each direction

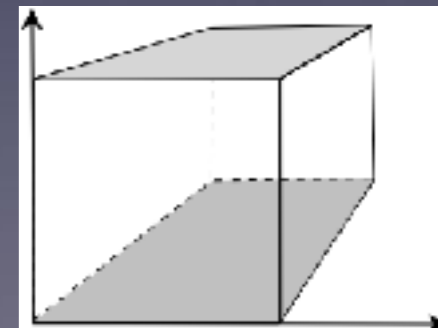
$$F_1 \rightarrow \langle U_\xi, V \rangle_N = \int_N UV \Big|_{\xi=-1}^1 d\eta d\zeta - \langle U, V_\xi \rangle_N$$



$$F_2 \rightarrow \langle U_\eta, V \rangle_N = \int_N UV \Big|_{\eta=-1}^1 d\xi d\zeta - \langle U, V_\eta \rangle_N$$



$$F_3 \rightarrow \langle U_\zeta, V \rangle_N = \int_N UV \Big|_{\zeta=-1}^1 d\xi d\eta - \langle U, V_\zeta \rangle_N$$



Discrete Gauss Law

$$\left(\nabla \cdot \vec{F}, \phi\right)_N = \int_{\partial E, N} \vec{F} \cdot \hat{n} dS - \left(\vec{F}, \nabla \phi\right)_N$$

Discrete Integral Calculus

$$\left(\nabla \cdot \vec{F}, \phi\right)_N = \int_{\partial E, N} \vec{F} \cdot \hat{n} dS - \left(\vec{F}, \nabla \phi\right)_N$$

$$\int_{E, N} \nabla \cdot \vec{F} d\xi = \int_{\partial E, N} \vec{F} \cdot \hat{n} dS$$

$$\left(\nabla^2 \Phi, V\right)_N + \left(\nabla \Phi, \nabla V\right)_N = \int_{\partial E, N} \nabla \Phi \cdot \hat{n} V dS$$

$$\left(\nabla^2 \Phi, V\right)_N - \left(\nabla^2 V, \Phi\right)_N = \int_{\partial E, N} (\nabla \Phi \cdot \hat{n} V - \nabla V \cdot \hat{n} \Phi) dS$$

From Exactness

$$\int_{E, N} \nabla V d\xi d\eta d\zeta = \int_{\partial E, N} V \hat{n} dS \qquad \int_{E, N} \nabla \times \vec{F} d\xi d\eta d\zeta = \int_{\partial E, N} \hat{n} \times \vec{F} dS$$

Coupling-Advective

Riemann Solver

$$\mathbf{F}^* (\mathbf{U}^L, \mathbf{U}^R) = \frac{\vec{\mathbf{f}} (\mathbf{U}^L) \cdot \hat{n} + \vec{\mathbf{f}} (\mathbf{U}^R) \cdot \hat{n}}{2} + \frac{\sigma}{2} |\bar{A}| (\mathbf{U}^L - \mathbf{U}^R)$$

$$= \left\{ \left\{ \vec{\mathbf{f}} \cdot \hat{n} \right\} \right\} - \frac{\sigma}{2} |\bar{A}| [[\mathbf{U}]]$$

Roe

Lax-Friedrichs

van Leer

...

Coupling - Diffusive

Bassi-Rebay-1:

$$\mathbf{U}^* (\mathbf{U}^L, \mathbf{U}^R) = \frac{\mathbf{U}^L + \mathbf{U}^R}{2} = \{\{\mathbf{U}\}\}$$

$$\mathbf{F}_v^* (\tilde{\mathbf{F}}_v^L \cdot \hat{n}, \tilde{\mathbf{F}}_v^R \cdot \hat{n}) = \{\{\tilde{\mathbf{F}}_v \cdot \hat{n}\}\}$$

Others...

Bassi-Rebay-2
Interior Penalty

...

Weak Form Construction...

Apply Gauss Law again...

$$\begin{aligned}
 & \langle \mathcal{J} \mathbf{u}_t, \phi \rangle + \int_{\partial E} \phi^T \left\{ \overset{\leftrightarrow}{\mathbf{F}}^* - \overset{\leftrightarrow}{\mathbf{f}} \cdot \hat{\mathbf{n}} - \frac{1}{\text{Re}} \overset{\leftrightarrow}{\mathbf{F}}_v^* \right\} dS - \langle \overset{\leftrightarrow}{\nabla}_\xi \cdot \overset{\leftrightarrow}{\mathbf{f}}, \phi \rangle = -\frac{1}{\text{Re}} \langle \overset{\leftrightarrow}{\mathbf{f}}_v, \overset{\leftrightarrow}{\nabla} \phi \rangle \\
 & \approx \langle \cdot, \cdot \rangle_N
 \end{aligned}$$

$\in \mathbb{P}^N$ $\in \mathbb{P}^N$ $\approx \int_{\partial E, N}$ $\approx \mathbb{D}(\mathbf{F}^\#) ???$

$$\begin{aligned}
 & \langle \mathcal{J} \overset{\leftrightarrow}{\mathbf{q}}, \overset{\leftrightarrow}{\psi} \rangle = \int_{\partial E} \{ \mathbf{U}^{*,T} - \mathbf{u} \} \{ \mathcal{M}^T \overset{\leftrightarrow}{\psi} \} \cdot \hat{\mathbf{n}} dS - \langle \mathbf{u}, \overset{\leftrightarrow}{\nabla} \cdot (\mathcal{M}^T \overset{\leftrightarrow}{\psi}) \rangle \\
 & \approx Q \in \mathbb{P}^N
 \end{aligned}$$

The diagram shows the mapping of terms from the top equation to the bottom equation. Yellow arrows indicate the following correspondences:

- $\langle \mathcal{J} \mathbf{u}_t, \phi \rangle$ maps to $\langle \mathcal{J} \overset{\leftrightarrow}{\mathbf{q}}, \overset{\leftrightarrow}{\psi} \rangle$ (labeled $\in \mathbb{P}^N$)
- $\int_{\partial E} \phi^T \{ \dots \} dS$ maps to $\int_{\partial E} \{ \mathbf{U}^{*,T} - \mathbf{u} \} \{ \mathcal{M}^T \overset{\leftrightarrow}{\psi} \} \cdot \hat{\mathbf{n}} dS$ (labeled $\approx \int_{\partial E, N}$)
- $\langle \overset{\leftrightarrow}{\nabla}_\xi \cdot \overset{\leftrightarrow}{\mathbf{f}}, \phi \rangle$ maps to $\langle \mathbf{u}, \overset{\leftrightarrow}{\nabla} \cdot (\mathcal{M}^T \overset{\leftrightarrow}{\psi}) \rangle$ (labeled $\approx \mathbb{D}(\mathbf{F}^\#) ???$)
- The right-hand side term $-\frac{1}{\text{Re}} \langle \overset{\leftrightarrow}{\mathbf{f}}_v, \overset{\leftrightarrow}{\nabla} \phi \rangle$ is associated with the label $\approx \langle \cdot, \cdot \rangle_N$.

Split Form/Two Point Flux

$$\vec{f} = \vec{A}(x)\mathbf{u}$$

$$\text{Split Form: } \nabla \cdot \vec{f} = \frac{1}{2} \left\{ \nabla \cdot \vec{f} + \vec{A} \cdot \nabla u + \nabla \cdot \vec{A}u \right\}$$

$$\frac{1}{2} \left(\nabla \cdot \vec{\mathbf{F}}(\mathbf{U}), \phi \right)_N + \frac{1}{2} \left(\mathbb{I}^N(\vec{\mathcal{A}}) \cdot \nabla \mathbf{U}, \phi \right)_N + \frac{1}{2} \left(\nabla \cdot \mathbb{I}^N(\vec{\mathcal{A}}) \mathbf{U}, \phi \right)_N$$

$$\phi = l_i l_j l_k$$

Volume Terms

$$\left(\nabla \cdot \vec{\mathbf{F}}(\mathbf{U}), \phi \right)_N \longrightarrow w_{ijk} \left\{ \sum_{n=0}^N F_{njk}^{(\xi)} \mathcal{D}_{in} + \sum_{n=0}^N F_{ink}^{(\eta)} \mathcal{D}_{jn} + \sum_{n=0}^N F_{ijn}^{(\zeta)} \mathcal{D}_{kn} \right\}$$

$$\left(\mathbb{I}^N(\vec{\mathcal{A}}) \cdot \nabla \mathbf{U}, \phi \right)_N \longrightarrow w_{ijk} \left\{ \mathcal{A}_{ijk}^{(\xi)} \sum_{n=0}^N \mathbf{U}_{njk} \mathcal{D}_{in} + \mathcal{A}_{ijk}^{(\eta)} \sum_{n=0}^N \mathbf{U}_{ink} \mathcal{D}_{jn} + \mathcal{A}_{ijk}^{(\zeta)} \sum_{n=0}^N \mathbf{U}_{ijn} \mathcal{D}_{kn} \right\}$$

$$\left(\nabla \cdot \mathbb{I}^N(\vec{\mathcal{A}}) \mathbf{U}, \phi \right)_N \longrightarrow w_{ijk} \left\{ \sum_{n=0}^N \mathcal{A}_{njk}^{(\xi)} \mathcal{D}_{in} + \sum_{n=0}^N \mathcal{A}_{ink}^{(\eta)} \mathcal{D}_{jn} + \mathcal{A}_{ijk}^{(\zeta)} \sum_{n=0}^N \mathcal{A}_{ijn}^{(\zeta)} \mathcal{D}_{kn} \right\} \mathbf{U}_{ijk}$$

Volume Terms

$$\frac{1}{2} \left(\nabla \cdot \vec{\mathbf{F}}(\mathbf{U}), \phi \right)_N + \frac{1}{2} \left(\mathbb{I}^N(\vec{\mathcal{A}}) \cdot \nabla \mathbf{U}, \phi \right)_N + \frac{1}{2} \left(\nabla \cdot \mathbb{I}^N(\vec{\mathcal{A}}) \mathbf{U}, \phi \right)_N$$



$$\begin{aligned} & \frac{1}{2} \sum_{n=0}^N \left\{ \mathbf{F}_{njk}^{(\xi)} + \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{njk} + \mathcal{A}_{njk}^{(\xi)} \mathbf{U}_{ijk} \right\} \mathcal{D}_{in} w_{ijk} \\ & + \frac{1}{2} \sum_{n=0}^N \left\{ \mathbf{F}_{ink}^{(\eta)} + \mathcal{A}_{ijk}^{(\eta)} \mathbf{U}_{ink} + \mathcal{A}_{ink}^{(\eta)} \mathbf{U}_{ijk} \right\} \mathcal{D}_{jn} w_{ijk} \\ & + \frac{1}{2} \sum_{n=0}^N \left\{ \mathbf{F}_{njk}^{(\zeta)} + \mathcal{A}_{ijk}^{(\zeta)} \mathbf{U}_{njk} + \mathcal{A}_{njk}^{(\zeta)} \mathbf{U}_{ijk} \right\} \mathcal{D}_{kn} w_{ijk} \\ & = \sum_{n=0}^N \bar{\mathbf{F}}_{(njk,i)}^{(\xi)} \mathcal{D}_{in} w_{ijk} + \sum_{n=0}^N \bar{\mathbf{F}}_{(ink,j)}^{(\eta)} \mathcal{D}_{jn} w_{ijk} + \sum_{n=0}^N \bar{\mathbf{F}}_{(ijn,k)}^{(\zeta)} \mathcal{D}_{kn} w_{ijk} \end{aligned}$$

Special Averages

$$\frac{1}{2} \sum_{n=0}^N \left\{ \mathbf{F}_{njk}^{(\xi)} + \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{njk} + \mathcal{A}_{njk}^{(\xi)} \mathbf{U}_{ijk} \right\} \mathcal{D}_{in}$$

+

$$\frac{1}{2} \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{ijk} \sum_{n=0}^N \mathcal{D}_{in} = \sum_{n=0}^N \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{ijk} \mathcal{D}_{in} = 0$$

= 0

$$= \frac{1}{2} \sum_{n=0}^N \left\{ \mathcal{A}_{njk}^{(\xi)} \mathbf{U}_{njk} + \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{njk} + \mathcal{A}_{njk}^{(\xi)} \mathbf{U}_{ijk} + \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{ijk} \right\} \mathcal{D}_{in}$$

Special Averages

$$= \frac{1}{2} \sum_{n=0}^N \left\{ \mathcal{A}_{njk}^{(\xi)} \mathbf{U}_{njk} + \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{njk} + \mathcal{A}_{njk}^{(\xi)} \mathbf{U}_{ijk} + \mathcal{A}_{ijk}^{(\xi)} \mathbf{U}_{ijk} \right\} \mathcal{D}_{in}$$

$$= 2 \sum_{n=0}^N \left\{ \left(\frac{\mathcal{A}_{njk}^{(\xi)} + \mathcal{A}_{ijk}^{(\xi)}}{2} \right) \left(\frac{\mathbf{U}_{njk} + \mathbf{U}_{ijk}}{2} \right) \right\} \mathcal{D}_{in}$$

$$= 2 \sum_{n=0}^N \left\{ \left\{ \mathcal{A}^{(\xi)} \right\} \right\}_{(n,i)jk} \left\{ \left\{ \mathbf{U} \right\} \right\}_{(n,i)jk} \mathcal{D}_{in}$$

$$= 2 \sum_{n=0}^N \mathbf{F}_{(n,i)jk}^{\#} \mathcal{D}_{in}$$

Key Ingredient

Summation-By-Parts and form of $\mathbf{F}^\#$ implies

$$\langle \mathbb{D}\mathbf{F}^\#, \mathbf{U} \rangle = \frac{1}{2} \int_{\partial E, N} \mathbf{U}^T \vec{\mathbf{F}} \cdot \hat{n} dS$$

Volume term replaced by surface quadrature

Control with numerical flux

DGSEM

$$\langle \mathcal{J}\mathbf{U}_t, \phi \rangle_N + \int_{\partial E, N} \phi^T \left\{ \tilde{\tilde{\mathbf{F}}}^* - \tilde{\tilde{\mathbf{f}}} \cdot \hat{\mathbf{n}} - \frac{1}{\text{Re}} \tilde{\tilde{\mathbf{F}}}_v^* \right\} dS - \langle \mathbb{D}(\tilde{\tilde{\mathbf{F}}}^\#), \phi \rangle_N = -\frac{1}{\text{Re}} \langle \tilde{\tilde{\mathbf{F}}}_v, \vec{\nabla} \phi \rangle_N$$

$$\langle \mathcal{J}\vec{\mathbf{Q}}, \vec{\psi} \rangle_N = \int_{\partial E, N} \{ \mathbf{U}^{**,T} - \mathbf{U} \} \{ \mathcal{M}^T \vec{\psi} \} \cdot \hat{\mathbf{n}} dS - \langle \mathbf{U}, \vec{\nabla} \cdot (\mathcal{M}^T \vec{\psi}) \rangle_N$$

Stability Analysis

$$\langle \mathcal{J}\mathbf{U}_t, \phi \rangle_N + \int_{\partial E, N} \phi^T \left\{ \vec{\tilde{\mathbf{F}}}^* - \vec{\mathbf{f}} \cdot \hat{\mathbf{n}} - \frac{1}{\text{Re}} \vec{\tilde{\mathbf{F}}}_v^* \right\} dS - \langle \mathbb{D}(\vec{\tilde{\mathbf{F}}}^\#), \phi \rangle_N = -\frac{1}{\text{Re}} \langle \vec{\tilde{\mathbf{F}}}_v, \vec{\nabla} \phi \rangle_N$$

$$\langle \mathcal{J}\vec{\mathbf{Q}}, \vec{\psi} \rangle_N = \int_{\partial E, N} \{ \mathbf{U}^{**,T} - \mathbf{U} \} \{ \mathcal{M}^T \vec{\psi} \} \cdot \hat{\mathbf{n}} dS - \langle \mathbf{U}, \vec{\nabla} \cdot (\mathcal{M}^T \vec{\psi}) \rangle_N$$

Linear

- Linearize equations
- Replace $\phi = (s^{-1})^T s^{-1} \mathbf{U}$
 $\psi \leftarrow \mathcal{B} \mathbf{Q}$
- Sum over all elements

Entropy

- Replace $\phi \leftarrow \mathbf{W}$
 $\psi \leftarrow \mathcal{B} \nabla \mathbf{W}$
(entropy variable)
- Sum over all elements

Linear Energy Bound

$$\frac{d}{dt} \sum_{elements} \|\mathbf{U}\|_{J,N}^2 \leq -2 \sum_{\substack{\text{Boundary} \\ \text{faces}}} \int_{\partial E,N} \left\{ \left[\tilde{\mathbf{F}}^* - \frac{1}{2} (\tilde{\mathbf{F}} \cdot \hat{n}) \right]^T \mathbf{U} - \frac{1}{\text{Re}} \left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} (\tilde{\mathbf{F}}_v \cdot \hat{n}) - \mathbf{U}^T (\tilde{\mathbf{F}}_v \cdot \hat{n}) \right] \right\} dS$$

Sufficient Condition for Stability:

$$\left[\tilde{\mathbf{F}}^* - \frac{1}{2} (\tilde{\mathbf{F}} \cdot \hat{n}) \right]^T \mathbf{U} - \frac{1}{\text{Re}} \left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} (\tilde{\mathbf{F}}_v \cdot \hat{n}) - \mathbf{U}^T (\tilde{\mathbf{F}}_v \cdot \hat{n}) \right] \geq 0$$

- 3D
- Curved Hex Elements
- Any Polynomial Order

BC Implementation

BC Implementations are stable if

$$(SSC) \quad \boxed{\left[\tilde{\mathbf{F}}^* - \frac{1}{2} (\tilde{\mathbf{F}} \cdot \hat{n}) \right]^T \mathbf{U}} - \frac{1}{\text{Re}} \boxed{\left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} (\tilde{\mathbf{F}}_v \cdot \hat{n}) - \mathbf{U}^T (\tilde{\mathbf{F}}_v \cdot \hat{n}) \right]} \geq 0$$

Dirichlet-Type

Neumann-Type

Robin-Type Conditions

A diagram with two arrows pointing downwards from the text 'Dirichlet-Type' and 'Neumann-Type' to the text 'Robin-Type Conditions'.

Typical Implementation

$$(E) \left[\tilde{\mathbf{F}}^* - \frac{1}{2} \left(\overset{\leftrightarrow}{\tilde{\mathbf{F}}} \cdot \hat{n} \right) \right]^T \mathbf{U} \geq 0 \quad \text{Euler Part}$$

$$(D) \left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} \left(\overset{\leftrightarrow}{\tilde{\mathbf{F}}}_v \cdot \hat{n} \right) - \mathbf{U}^T \left(\overset{\leftrightarrow}{\tilde{\mathbf{F}}}_v \cdot \hat{n} \right) \right] \leq 0 \quad \text{Navier-Stokes Part}$$

Sufficient, but not necessary

Examples

- Euler Inflow/Outflow
- Euler Free-Slip Wall
- Navier-Stokes Inflow-Outflow
- Navier-Stokes Wall

Linear-Symmetric Equations

$$\mathbf{U} = \begin{bmatrix} \rho \\ U \\ V \\ W \\ P \end{bmatrix} \quad \vec{\mathbf{F}} \cdot \hat{\mathbf{n}} = \begin{bmatrix} b\mathbb{N} \\ n_x(\rho b + aP) \\ n_y(\rho b + aP) \\ n_z(\rho b + aP) \\ a\mathbb{N} \end{bmatrix} \quad \mathbb{N} = (U, V, W) \cdot \hat{\mathbf{n}}$$

$a^2 + b^2 = c^2$

Euler Inflow-Outflow



Specify Free Stream in Upwind Riemann Solver

$$\tilde{\mathbf{F}}^*(\mathbf{U}^L, \mathbf{U}^R) = \left\{ \left\{ \tilde{\mathbf{A}} \cdot \hat{n} \mathbf{U} \right\} \right\} - \frac{|\tilde{\mathbf{A}} \cdot \hat{n}|}{2} \left[\left[\mathbf{U} \right] \right] = A^+ \mathbf{U}^L + A^- \mathbf{U}^R$$

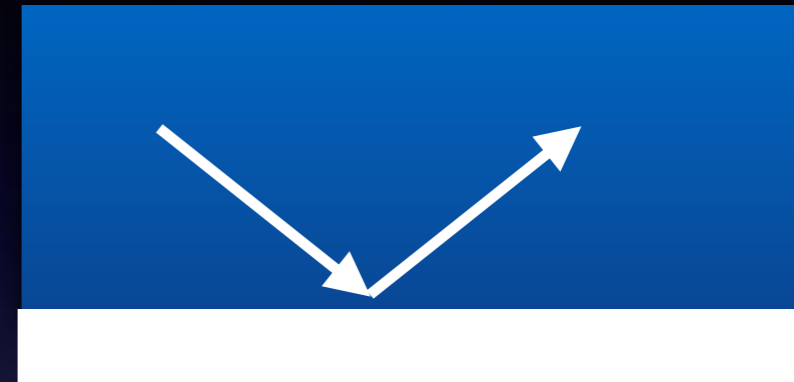
$$(E) \quad \left(\tilde{\mathbf{F}}^* - \frac{1}{2} \tilde{\mathbf{F}} \cdot \hat{n} \right)^T \mathbf{U} \geq \frac{1}{2} \mathbf{U}^T \underline{\mathbf{A}}^+ \mathbf{U} \geq 0 \quad \checkmark$$

Euler Free-Slip Wall

Specify No
Normal Velocity

$$\mathbb{N} = (U, V, W) \cdot \hat{n} = 0$$

$$\mathbf{F}^* = \begin{bmatrix} 0 \\ n_x (b\rho + aP) \\ n_y (b\rho + aP) \\ n_z (b\rho + aP) \\ 0 \end{bmatrix}$$

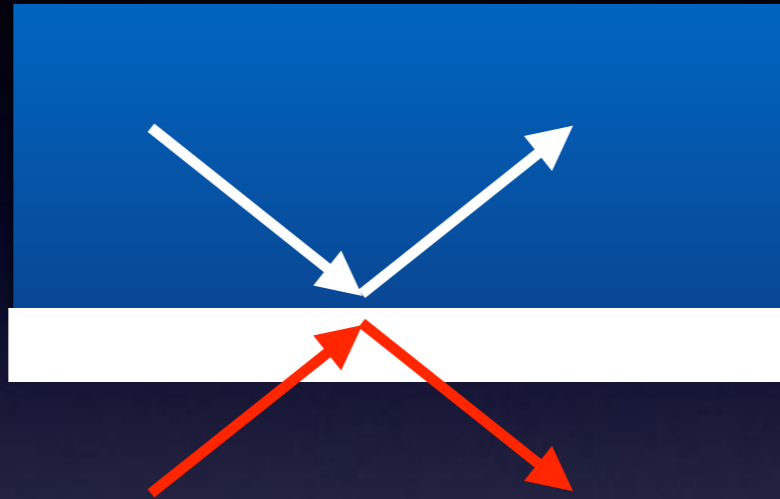


$$(E) \quad \mathbf{U}^T \left(\mathbf{F}^* - \frac{1}{2} \mathbf{F} \cdot \hat{n} \right) = \begin{bmatrix} \rho & U & V & W & P \end{bmatrix} \begin{bmatrix} -b\mathbb{N} \\ n_x (b\rho + aP) \\ n_y (b\rho + aP) \\ n_z (b\rho + aP) \\ -a\mathbb{N} \end{bmatrix} = 0$$



Euler Free-Slip Wall

Equal & Opposite in
Upwind Riemann
Solver

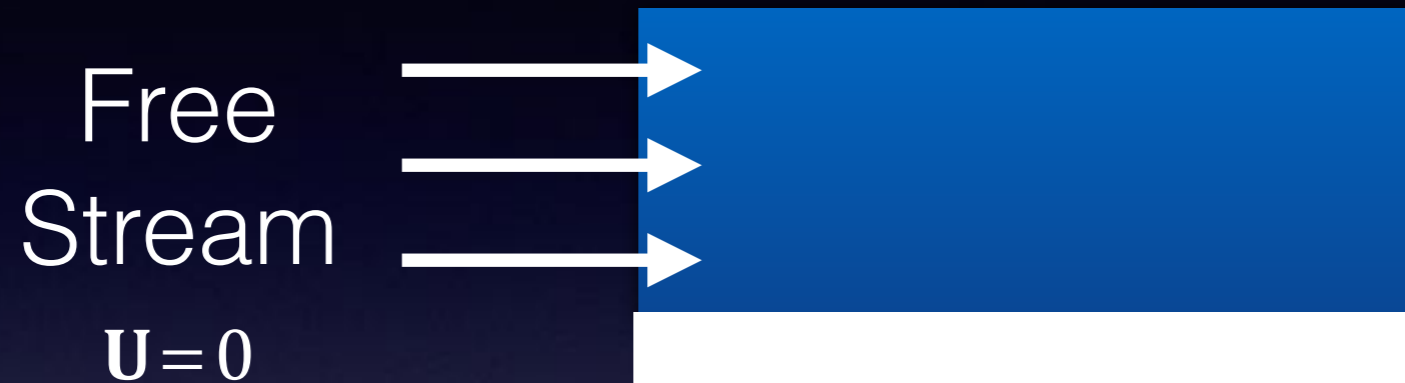


$$(\mathbf{v} \cdot \hat{\mathbf{n}})^{ext} \equiv \mathbb{N}^{ext} = -(\mathbf{v} \cdot \hat{\mathbf{n}})^{int} \equiv -\mathbb{N}^{int}$$

$$\tilde{\mathbf{F}}^*(\mathbf{U}^L, \mathbf{U}^R) = \left\{ \left\{ \tilde{\mathbf{A}} \cdot \hat{\mathbf{n}} \mathbf{U} \right\} \right\} - \frac{|\tilde{\mathbf{A}} \cdot \hat{\mathbf{n}}|}{2} \left[\left[\mathbf{U} \right] \right] = A^+ \mathbf{U}^L + A^- \mathbf{U}^R$$

$$(E) \quad \left(\tilde{\mathbf{F}}^* - \frac{1}{2} \tilde{\mathbf{F}} \cdot \hat{\mathbf{n}} \right)^T \mathbf{U} = c \mathbb{N}^2 \geq 0 \quad \checkmark$$

Navier-Stokes Inflow



Specify Ext State

$$(E) \left(\tilde{\mathbf{F}}^* - \frac{1}{2} \tilde{\mathbf{F}} \cdot \hat{n} \right)^T \mathbf{U} \geq \frac{1}{2} \mathbf{U}^T \underline{\mathbf{A}}^+ \mathbf{U} \geq 0 \quad \checkmark$$

$$(D) \left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) - \mathbf{U}^T \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) \right]$$

Navier-Stokes Inflow

$$(D) \quad \left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} \left(\tilde{\mathbf{F}}_v \cdot \hat{\mathbf{n}} \right) - \mathbf{U}^T \left(\tilde{\mathbf{F}}_v \cdot \hat{\mathbf{n}} \right) \right] = 0 \quad \checkmark$$

$$\tilde{\mathbf{F}}_v^* = \tilde{\mathbf{F}}_v \cdot \hat{\mathbf{n}}$$

Compute Flux
from Interior

$$\mathbf{U}^* = 0$$

Specify Solution

$$(E) + (D) = \left(\tilde{\mathbf{F}}^* - \frac{1}{2} \tilde{\mathbf{F}} \cdot \hat{\mathbf{n}} \right)^T \mathbf{U} \geq \frac{1}{2} \mathbf{U}^T \underline{\mathbf{A}}^+ \mathbf{U} \geq 0$$

Navier-Stokes Outflow



$$(E) \left(\tilde{\mathbf{F}}^* - \frac{1}{2} \tilde{\mathbf{F}} \cdot \hat{n} \right)^T \mathbf{U} \geq \frac{1}{2} \mathbf{U}^T \underline{\mathbf{A}}^+ \mathbf{U} \geq 0 \quad \checkmark$$

$$(D) \left[\tilde{\mathbf{F}}_v^{*,T} \mathbf{U} + \mathbf{U}^{*,T} \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) - \mathbf{U}^T \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) \right] = 0 \quad \checkmark$$

$$\tilde{\mathbf{F}}_v^* = 0$$

Specify Flux

$$\mathbf{U}^* = \mathbf{U}$$

Use interior Solution

Navier-Stokes Wall

Satisfy (E) through Riemann Solver

Re-Write (D)

$$\mathbf{U}^T \tilde{\mathbf{F}}_v^* + \mathbf{U}^{*,T} \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) - \mathbf{U}^T \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) = \mathbf{U}^T \left\{ \tilde{\mathbf{F}}_v^* - \tilde{\mathbf{F}}_v \cdot \hat{n} \right\} + \mathbf{U}^{*,T} \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) \leq 0$$

Written out...

$$\begin{bmatrix} \rho & U & V & W & P \end{bmatrix} \begin{bmatrix} 0 \\ \tau_1^* - \tau_1 \\ \tau_2^* - \tau_2 \\ \tau_3^* - \tau_3 \\ r \left(\frac{\partial P^*}{\partial n} - \frac{\partial P}{\partial n} \right) \end{bmatrix} + \begin{bmatrix} \rho^* & U^* & V^* & W^* & P^* \end{bmatrix} \begin{bmatrix} 0 \\ \tau_1 \\ \tau_2 \\ \tau_3 \\ r \frac{\partial P}{\partial n} \end{bmatrix} \leq 0,$$

$$\tau_i = n_x \tau_{i1} + n_y \tau_{i2} + n_z \tau_{i3}$$

Navier-Stokes Wall

$$\begin{bmatrix} \rho & U & V & W & P \end{bmatrix} \begin{bmatrix} 0 \\ \tau_1^* - \tau_1 \\ \tau_2^* - \tau_2 \\ \tau_3^* - \tau_3 \\ r \left(\frac{\partial P^*}{\partial n} - \frac{\partial P}{\partial n} \right) \end{bmatrix} + \begin{bmatrix} \rho^* & U^* & V^* & W^* & P^* \end{bmatrix} \begin{bmatrix} 0 \\ \tau_1 \\ \tau_2 \\ \tau_3 \\ r \frac{\partial P}{\partial n} \end{bmatrix} \leq 0,$$

Vanishes if

$$\tau_i^* = \tau_i$$

$$U^* = V^* = W^* = 0$$

+

Isothermal

$$P^* = 0$$

$$\frac{\partial P^*}{\partial n} = \frac{\partial P}{\partial n}$$

Adiabatic

$$P^* = P$$

$$\frac{\partial P^*}{\partial n} = 0$$

Not so fast...

A Guide to the Implementation of Boundary Conditions... AIAA 2014

Use interior Solution $\mathbf{U}^* = \mathbf{U}$

Viscous Flux from Interior: $\tilde{\mathbf{F}}_v^* = \tilde{\mathbf{F}}_v \cdot \hat{n}$

$$\text{(SSC)} \quad \underbrace{\left\{ \tilde{\mathbf{F}}^* - \frac{1}{2} \left(\tilde{\mathbf{F}} \cdot \hat{n} \right) \right\}^T \mathbf{U}}_{\geq 0} - \frac{1}{\text{Re}} \underbrace{\left\{ \mathbf{U}^T \left(\tilde{\mathbf{F}}_v \cdot \hat{n} \right) \right\}}_{\text{???}} \geq \text{???}$$

Nonlinear: Entropy Bound

$$\begin{aligned} \frac{d}{dt} \bar{S} \leq & - \sum_{\substack{\text{Boundary} \\ \text{faces}}} \int_N \left\{ (\mathbf{W})^T \left(\tilde{\mathbf{F}}^{\text{ec},*} - \left(\overset{\leftrightarrow}{\mathbf{F}} \cdot \hat{n} \right) \right) + \left(\overset{\leftrightarrow}{F}^\epsilon \cdot \hat{n} \right) \right\} dS \\ & + \frac{1}{\text{Re}} \sum_{\substack{\text{Boundary} \\ \text{faces}}} \int_N \left\{ \mathbf{W}^T \left(\tilde{\mathbf{F}}_v^* - \left(\overset{\leftrightarrow}{\mathbf{F}}_v \cdot \hat{n} \right) \right) + (\mathbf{W}^*)^T \left(\overset{\leftrightarrow}{\mathbf{F}}_v \cdot \hat{n} \right) \right\} dS, \end{aligned}$$

Sufficient Condition for Stability

$$- \left\{ (\mathbf{W})^T \left(\tilde{\mathbf{F}}^{\text{ec},*} - \left(\overset{\leftrightarrow}{\mathbf{F}} \cdot \hat{n} \right) \right) + \left(\overset{\leftrightarrow}{F}^\epsilon \cdot \hat{n} \right) \right\} + \frac{1}{\text{Re}} \left\{ \mathbf{W}^T \left(\tilde{\mathbf{F}}_v^* - \left(\overset{\leftrightarrow}{\mathbf{F}}_v \cdot \hat{n} \right) \right) + (\mathbf{W}^*)^T \left(\overset{\leftrightarrow}{\mathbf{F}}_v \cdot \hat{n} \right) \right\} \leq 0$$

TO DO

- Robin Conditions
- Entropy BCs

Issues: Linear theory well understood

Linear Stability \nleftrightarrow Nonlinear Stability

Entropy function not unique

A stable procedure with one entropy function may not be stable with another.

Summary

Have linear and entropy stability bounds to establish stability of DGSEM Approximations for

- Arbitrary 3D geometries
- Curved elements
- Any polynomial order

Bounds establish stable boundary procedures

Approach extends to, Shallow water, MHD eqns., ...

See Andrew's talk